

# COMPACTION INNOVATIONS AND CONTROL BASED ON SOIL MODULUS

By  
Jean-Louis BRIAUD

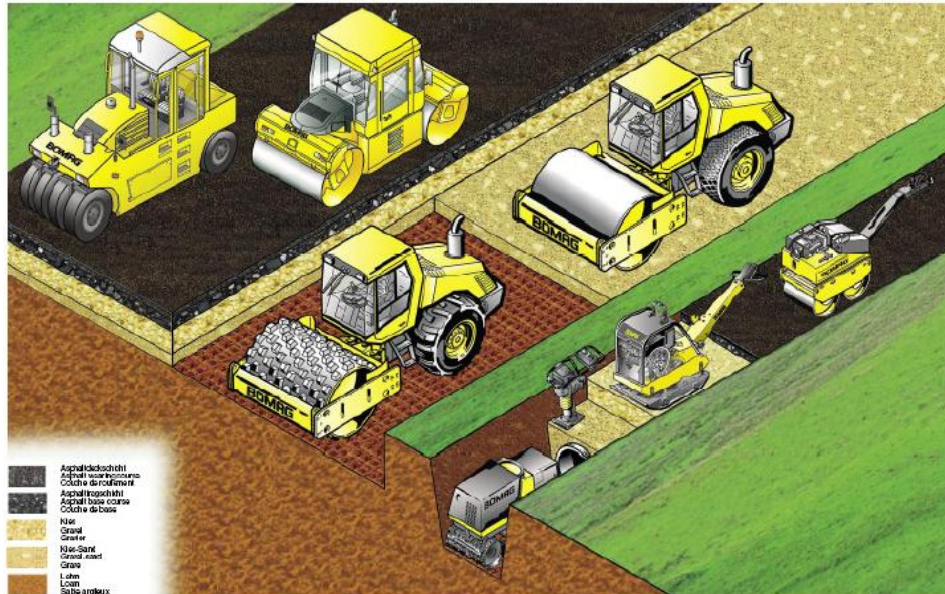
President of ISSMGE  
Professor, Texas A&M University, USA

J-L Briaud, Texas A&M University

## ACKNOWLEDGEMENTS

- Hans Kloubert, BOMAG
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- Kukjo Kim, Texas A&M Univ.
- Jeongbok Seo, Texas A&M Univ.

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**Current compaction practice**

**Future practice**

**Modulus and dry density**

**Intelligent compaction**

**Non cylindrical roller compaction**

## CURRENT PRACTICE

### Based on Density

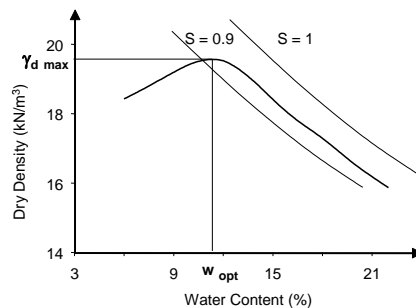
- LAB: Proctor test to get dry density vs. water content curve
- SPEC:  $x\%$  of  $\gamma_{d \max}$  within range of  $w_{\text{opt}}$
- FIELD: Compact and check that  $\gamma_d$  and  $w$  meet the specs

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## CURRENT PRACTICE

### Based on Density

- LAB : Proctor Test



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## CURRENT PRACTICE

### Based on Density

- SPECIFICATIONS.

X % of  $\gamma_{d \text{ max}}$  within range of  $w_{\text{opt}}$

- FIELD



Nuclear Density Meter  
For  $\gamma_d$  and  $w$

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## Dry Density: Advantages and Disadvantages

### 1. Advantages

Accumulated knowledge  
Well defined parameter  
Indication of solids per unit volume

### 2. Disadvantages

Not related to design  
Not very sensitive  
Not easy to measure quickly in field

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## FUTURE PRACTICE

### Based on Modulus

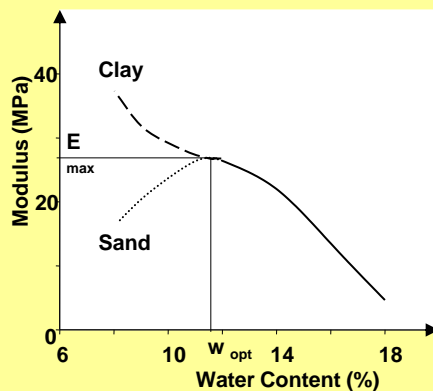
- LAB: Modulus test to get modulus vs. water content curve
- SPEC:  $x\%$  of  $E_{\max}$   
within range of  $w_{\text{opt}}$
- FIELD: Intelligent compaction and check that  $E_{\max}$  and  $w$  meet the specs

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## FUTURE PRACTICE

### Based on Modulus

- LAB : Modulus Test



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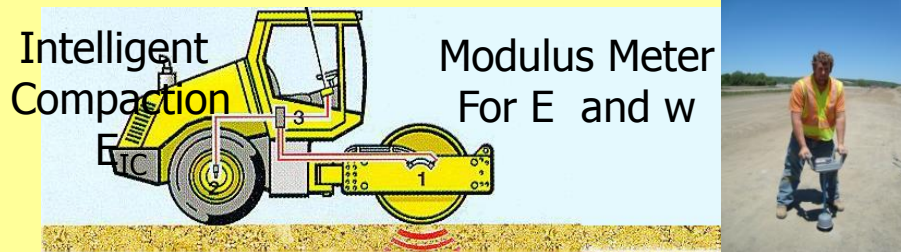
## FUTURE PRACTICE

### Based on Modulus

- SPECIFICATIONS

X % of  $E_{\max}$  within range of  $w_{\text{opt}}$

- FIELD



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## Modulus: Advantages and Disadvantages

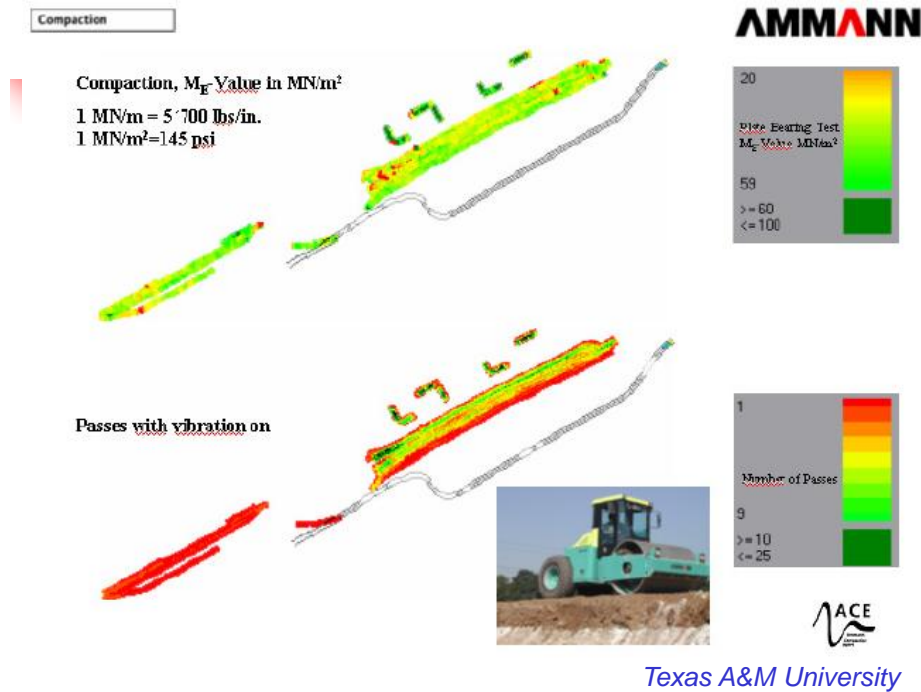
### 1. Advantages

Directly related to design  
Very sensitive to water content  
Easy to measure quickly in field

### 2. Disadvantages

Many influencing factors  
No lab test to get E vs. w  
No target values  
New concept

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## Stiffness or Modulus?

$$K = F/x \quad \text{in MN/m}$$

$$E \sim \sigma/\epsilon \quad \text{in MN/m}^2 \text{ or MPa}$$

$$E = \alpha F/Bx$$

$$K = F/x = EB/\alpha$$

## Stiffness or Modulus?

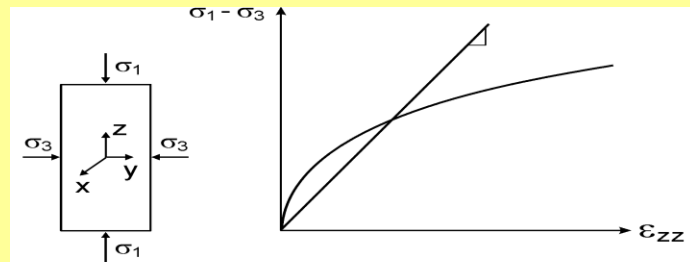
Stiffness depends on the size of the roller.

Modulus does not; it is a property of the soil only.

**Use the modulus, not the stiffness**

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## CALCULATION OF MODULUS



$$\epsilon_{xx} = \frac{1}{E} (\sigma_{xx} - \nu(\sigma_{yy} + \sigma_{zz})) = \frac{1}{E} (\sigma_3 - \nu(\sigma_1 + \sigma_3)) \quad (1)$$

$$\epsilon_{yy} = \frac{1}{E} (\sigma_{yy} - \nu(\sigma_{xx} + \sigma_{zz})) = \frac{1}{E} (\sigma_3 - \nu(\sigma_1 + \sigma_3)) \quad (2)$$

$$\epsilon_{zz} = \frac{1}{E} (\sigma_{zz} - \nu(\sigma_{xx} + \sigma_{yy})) = \frac{1}{E} (\sigma_1 - \nu(\sigma_3 + \sigma_3)) \quad (3)$$

$$E = \frac{\sigma_1 - 2\nu \sigma_3}{\epsilon_{zz}} \quad (4)$$

$$\frac{\epsilon_{xx}}{\epsilon_{zz}} = \frac{\sigma_3 - \nu(\sigma_1 + \sigma_3)}{\sigma_1 - 2\nu \sigma_3} \quad (5)$$

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# Which Modulus?

## DEFINITION

Initial

Secant

Tangent

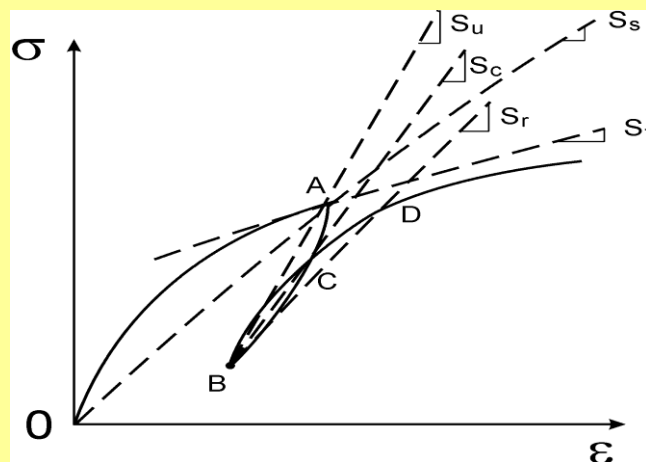
Unload-Resilient

Cyclic

Reload

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# WHICH MODULUS?



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## Which Modulus?

### STATE FACTORS

Density

Structure

Water content

Stress history

Cementation

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## Which Modulus?

### LOADING FACTORS

Stress level

Strain level

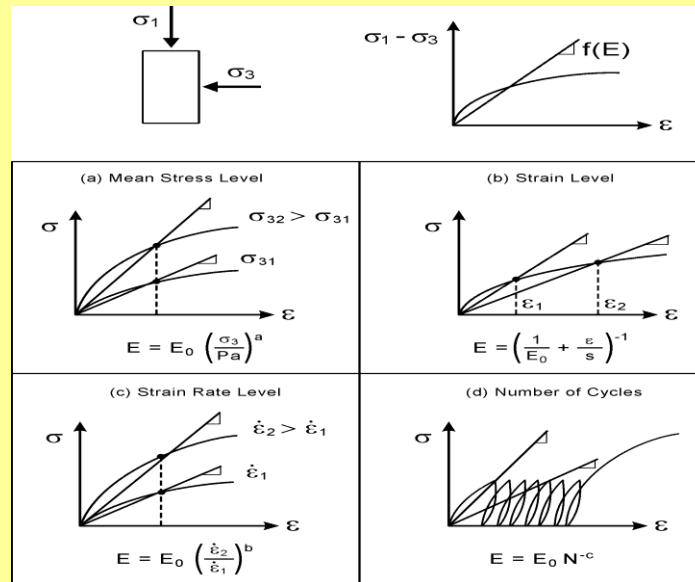
Strain rate

Number of cycles

Drainage

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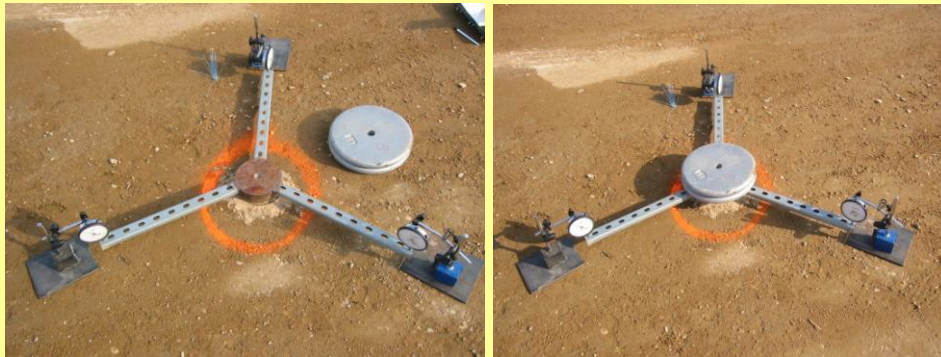
## WHICH MODULUS?



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## Which Modulus?

### PLATE MODULUS in FIELD

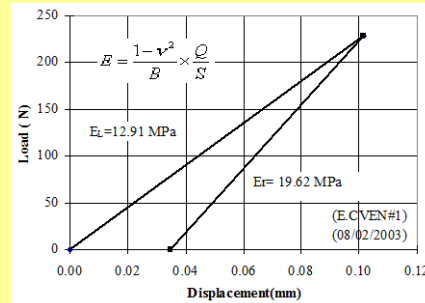


**BPT: Briaud Plate Test**

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# Which Modulus?

## PLATE MODULUS in LAB



### BPT: Briaud Plate Test

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## Range of Modulus

Steel:	200,000 MPa
Concrete:	20,000 MPa
Wood, Plastic:	13,000 MPa
Rock:	2,000 to 30,000 MPa
Asphalt:	150 to 25000 MPa
Soil:	5 MPa to 1000 MPa
Mayonnaise:	0.5 MPa

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# Asphalt Modulus

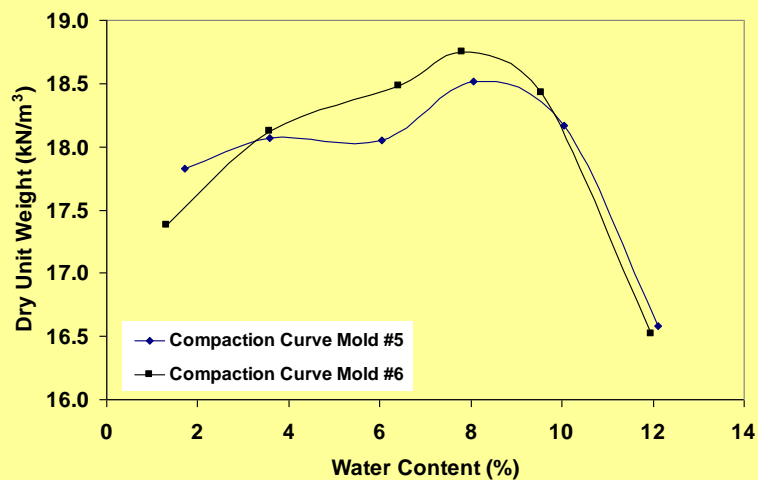
150 to 300 MPa at 140°C

3000 to 4500 MPa at 20°C

25000 MPa at -10°C

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# NGES Sand



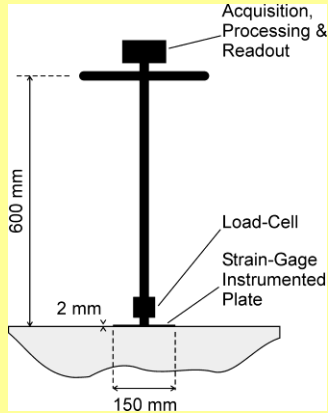
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## Example of same modulus test in lab and in field

### BCD Test: Briaud Compaction Device

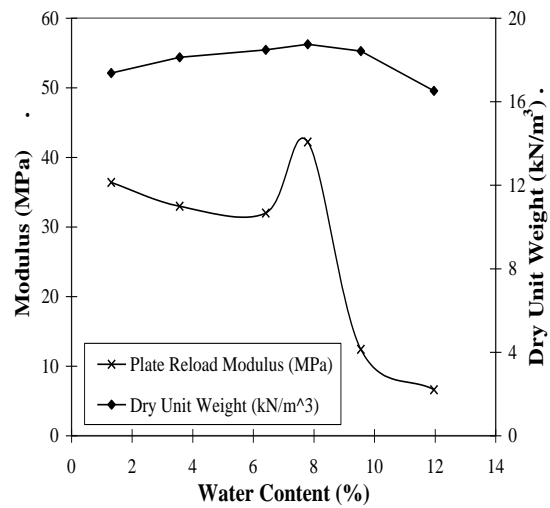


BCD on Proctor Mold

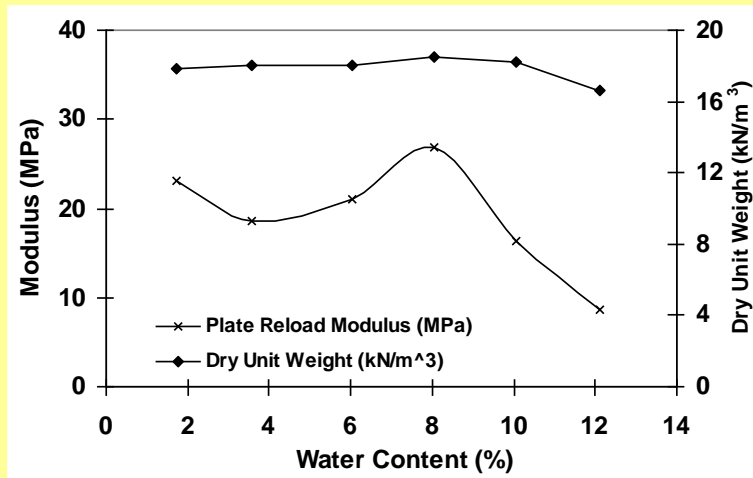


BCD in the Field

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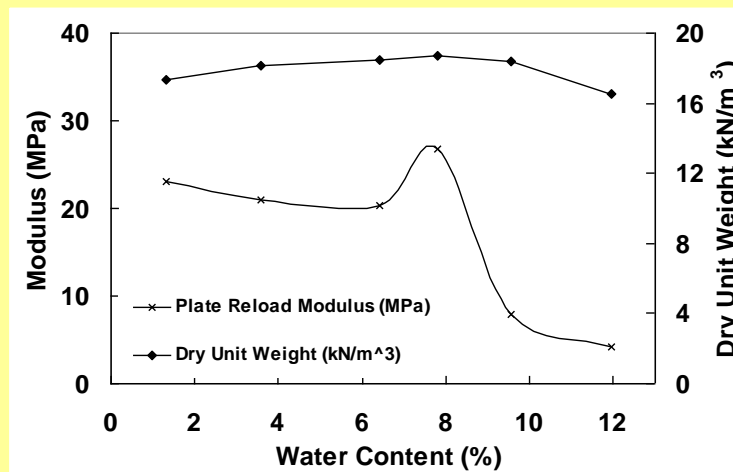
## NGES Silty Sand (Mold #5)



Modulus measured with BPT: Briaud Plate Test

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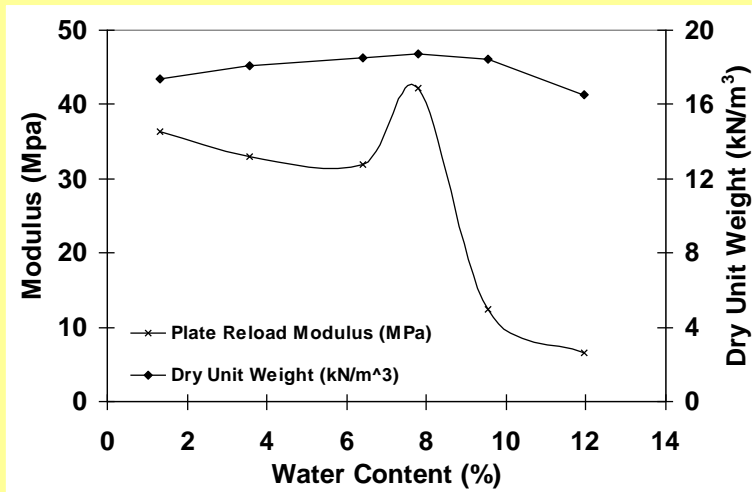
## NGES Silty Sand (Mold #6)



Modulus measured with BPT: Briaud Plate Test

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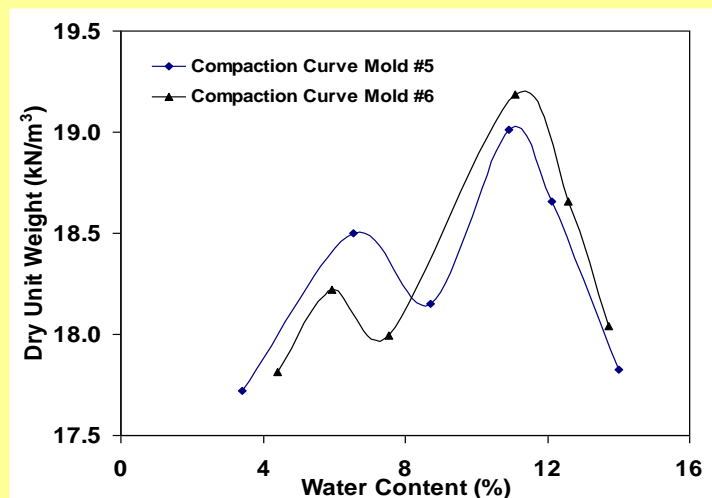
## NGES Silty Sand



Modulus measured with BPT: Briaud Plate Test

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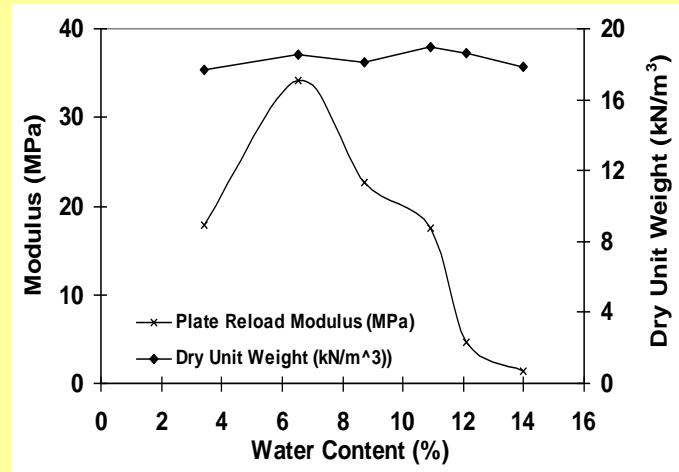
## NGES Sand + Porcelain Clay



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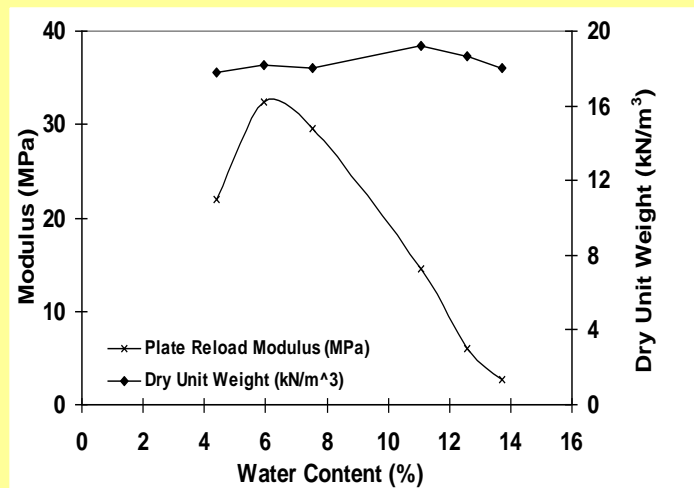
## NGES Sand + Porcelain Clay (Mold #5)



Modulus measured with BPT: Briaud Plate Test

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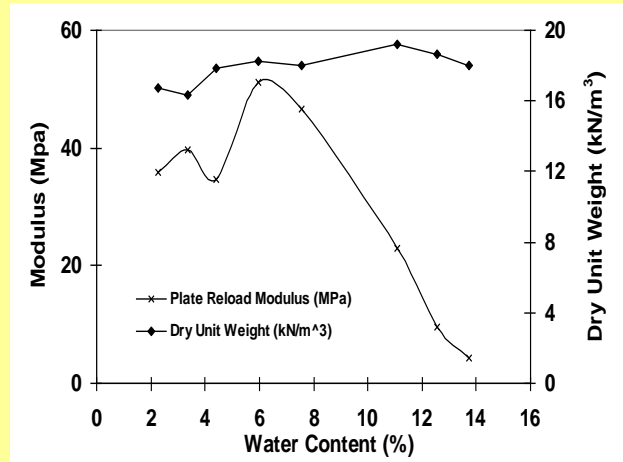
## NGES Sand + Porcelain Clay (Mold #6)



Modulus measured with BPT: Briaud Plate Test

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## NGES Sand + Porcelain Clay



Modulus measured with BPT: Briaud Plate Test

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1. Density?
2. Modulus?
3. Water Content?

- Only one of those three is not enough
- Two of those three are sufficient
- All three would be nice

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# Compaction Control Methods

- Conventional Compaction
- Intelligent Compaction
- Non cylindrical Compaction

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## Conventional Compaction (static or vibratory smooth drum or sheep-foot)



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## Intelligent Compaction



## Non Cylindrical Compaction



# Intelligent Vibratory Compaction

- Instrumented vibrating rollers
- Measure roller accel. as a function of time
- Calculate a soil modulus
- That modulus is/not independent of the roller
- Intelligent roller modifies automatically & instantaneously its own settings (force, ampl., freq.) to meet the target modulus

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## History

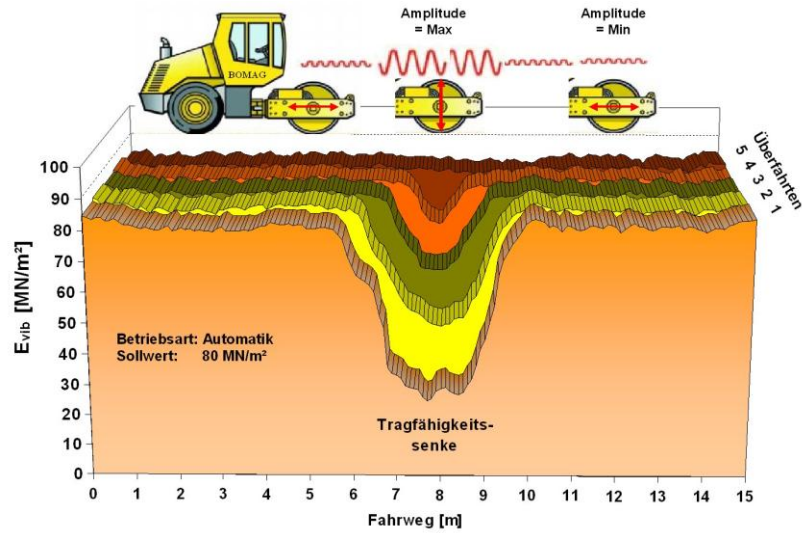
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- First “Intelligent Compaction” Compactor: 1992
- BOMAG (Germany)
- AMMANN Compaction Expert (ACE, Switzerland)
- Geodynamik (Sweden)

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# BOMAG

Recompaction of soft formation area with VARIOCONTROL automatic mode, presetting ( target value )  $E_{VIB} = 80 \text{ MN/m}^2$



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## Intelligent Compaction

## AMMANN



Intelligent Compaction  
Tests in the U.S.A.

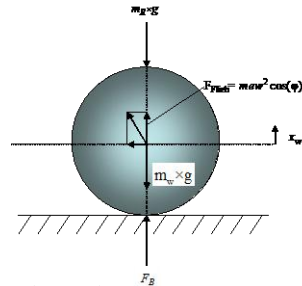


$\ddot{x}_d$ 

## From Acceleration to Stiffness

$$F_B \cong -m_d \ddot{x}_d + m_u r_u \Omega^2 \cos(\Omega t) + (m_f + m_d)g$$

$$F_B \cong k_B x_d + d_B \dot{x}_d$$



$F_B$ : soil-drum-interaction-force

$x_d$ : vert. disp. of drum (m)

$m_f$ : mass of the frame (kg)

$r_u$ : radial distance for  $m_u$

$g$ : acc. due to gravity (m/sec<sup>2</sup>)

$\dot{x}_d$ : velocity of drum

$d_B$ : damping coefficient ( $d_B \sim 0.2$ )

$m_d$ : mass of the drum (kg)

$\ddot{x}_d$ : acceleration of drum

$m_u$ : unbalanced mass (kg)

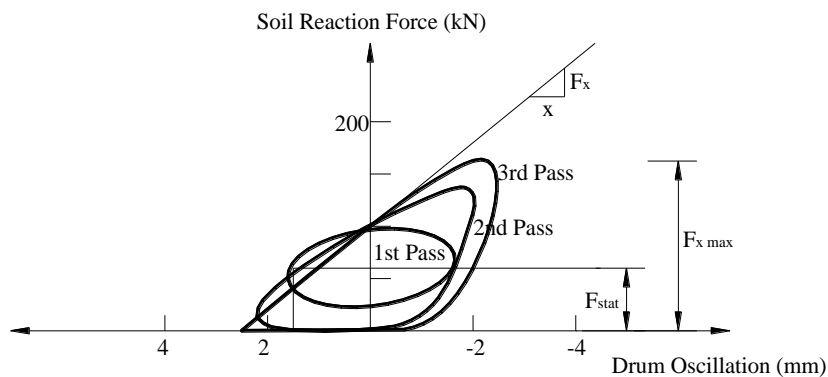
$\Omega = 2\pi f$

$f$ : frequency of rotating shaft (Hz)

$k_B$ : stiffness of soil

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## Force-Displacement Curves



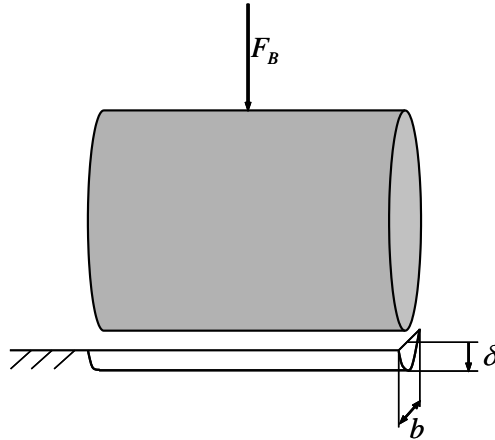
From BOMAG

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$\ddot{x}_d$ 

## From Stiffness to Modulus



H. Hertz, 1895 :

$$b = \sqrt{\frac{16}{\pi} \cdot \frac{R(1-\nu^2)}{E} \cdot \frac{F_B}{l}}$$

G. Lundberg, 1939 :

$$\delta = \frac{1-\nu^2}{E} \cdot \frac{F_B}{l} \cdot \frac{2}{\pi} \cdot (1,8864 + \ln \frac{l}{b})$$

$$\delta = f(F_B, E)$$

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 $\ddot{x}_d$ 

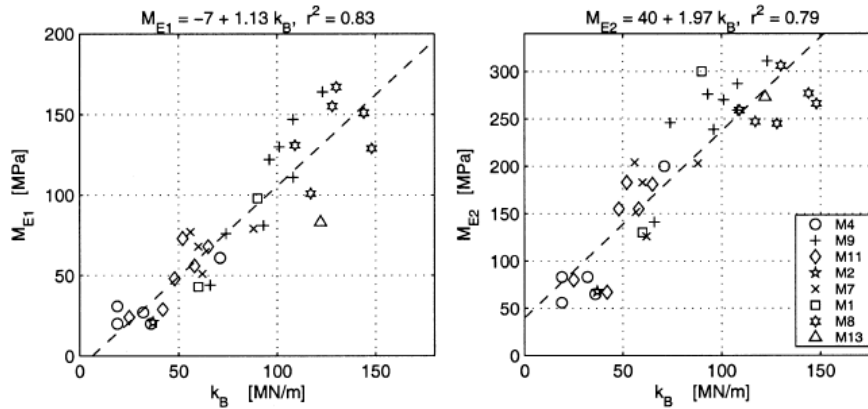
## From Stiffness to Modulus (theoretical)

$$k_B = \frac{E \cdot L \cdot \pi}{2 \cdot (1-\nu^2) \cdot \left( 2.14 + \frac{1}{2} \cdot \ln \left[ \frac{\pi \cdot L^3 \cdot E}{(1-\nu^2) \cdot 16 \cdot (m_f + m_d) \cdot R \cdot g} \right] \right)} \quad [\text{MN/m}]$$

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## From Stiffness to Modulus (experimental)



From AMMANN

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## Soil Modulus for Intelligent Compaction

**Soil:**    **5 MPa unacceptable**  
              **200 MPa excellent**

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## Specifications based on Modulus

Laying and compaction specification for  
road construction in Germany

<b>Soil layers</b>	<b>Density</b> (Standard Proctor)	<b>Bearing capacity</b> (load bearing test, EV2)	<b>Eveness</b> (4 m straight edge)
<b>Subbase</b>	<b>100 - 103 % *</b>	<b>100 - 150 MN/m<sup>2</sup> *</b>	<b>20 mm</b>
<b>Capping layer</b>	<b>100 - 103 % *</b>	<b>100 - 120 MN/m<sup>2</sup> *</b>	<b>40 mm</b>
<b>Formation</b>	<b>97 - 100 % *</b>	<b>45 - 80 MN/m<sup>2</sup> *</b>	<b>60 mm</b>

\* depending on road classification and road design

**From BOMAG**

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## Why Intelligent Compaction?

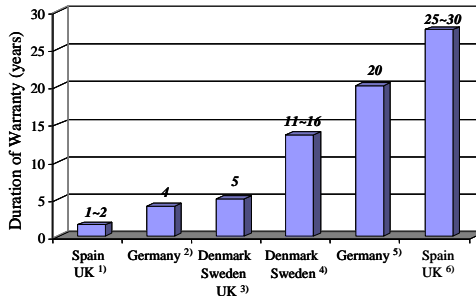
### □ TYPE OF CONTRACTS (EUROPE)

- Best-value awards rather than low bid
- Design-build rather than prescriptive specifications
- Performance contracting
- Continuous Compaction Control (CCC) in national standards: Austria (RVS 8S.02.6), Germany (ZTVE StB94), Sweden (VÄG 94), and Finland

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## Why Intelligent Compaction?

### WARRANTY



- 1) Material and Workmanship
- 2) Material and Workmanship
- 3) Performance
- 4) Pavement Performance Contracts
- 5) Pavement Performance Contracts "Functional"
- 6) Design-Build Finance Operate

### ECONOMICS

- More than 30% reduction in labor time and fuel costs
- Reduce the number of conventional spot tests
- Increase the roller's useful life

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## ISSUES

1. Reference modulus = plate test?
2. Develop simple lab modulus test
3. Study modulus vs water/asph. Content
4. Demonstrate that IC is better than CC
5. Calibrate rollers against plate modulus
6. Use same modulus test (lab and field)

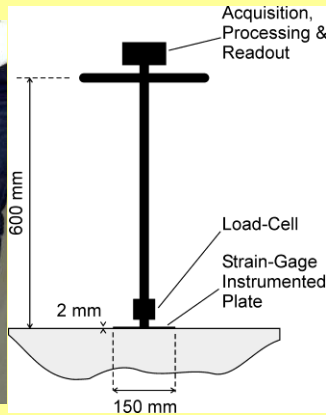
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## Example of same modulus test in lab and in field

### BCD Test: Briaud Compaction Device



BCD on Proctor Mold



BCD in the Field

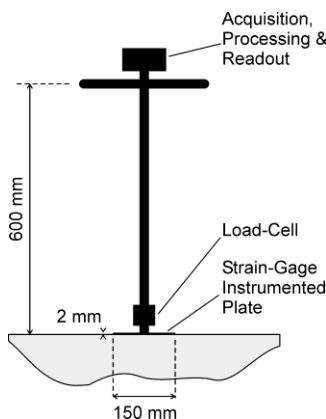
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## Example of same modulus test in lab and in field

### BCD Test: Briaud Compaction Device



BCD on Proctor Mold



BCD in the Field

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## ISSUES

7. Develop specs based on modulus for diff. pavement cond.
8. Can the asphalt modulus be isolated from the soil modulus
9. Use modulus control equipment
10. Demonstrate the IC equipment
11. First International Conference on Compaction?

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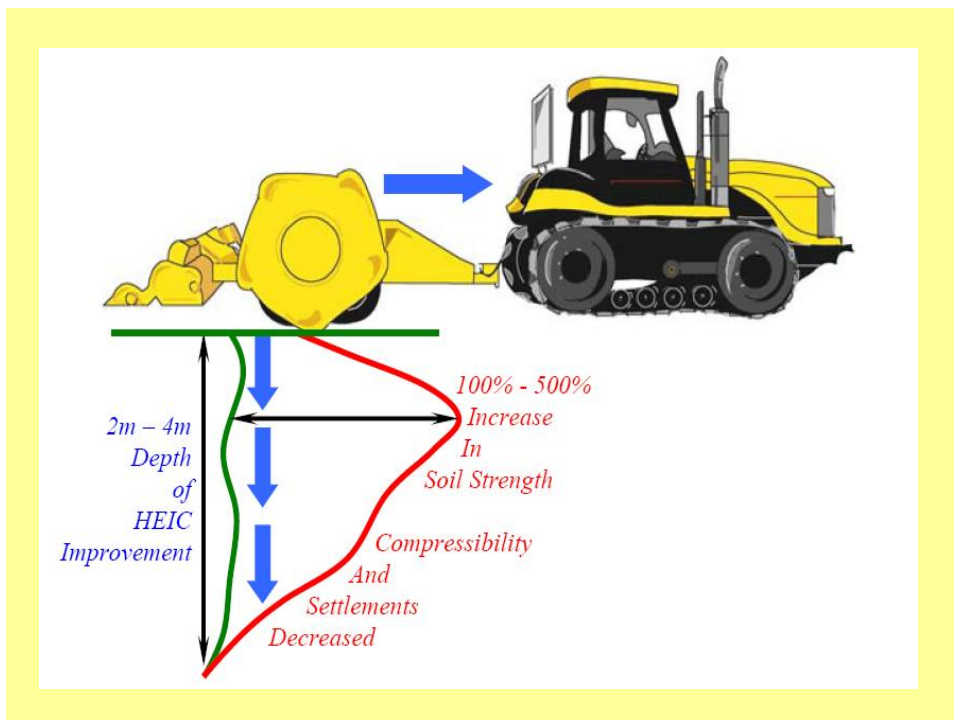
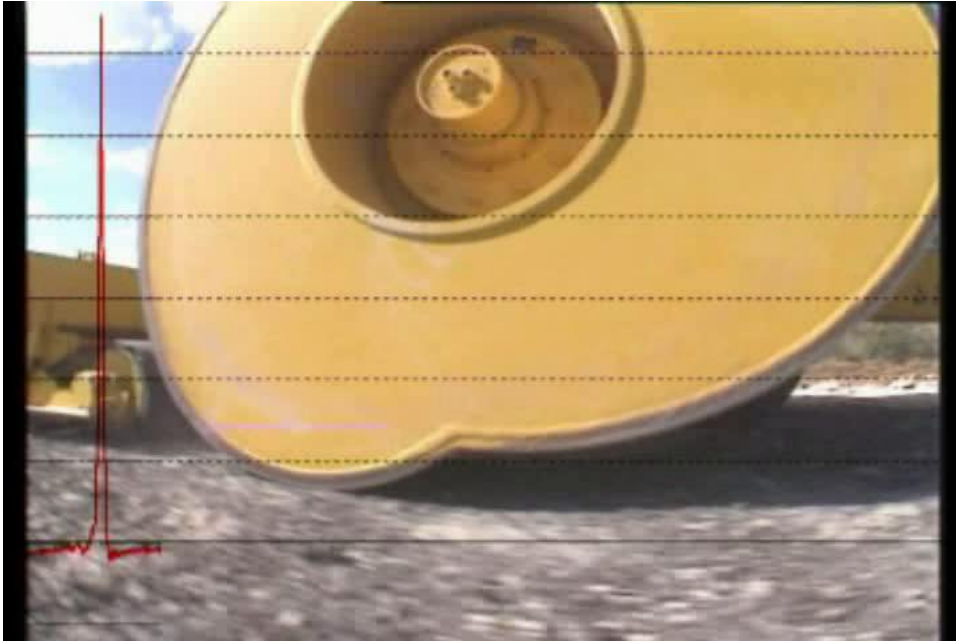
## Non cylindrical compaction

- Triangular and polygonal rollers
- Impact generated
- Landpac
- Broons
- Bomag

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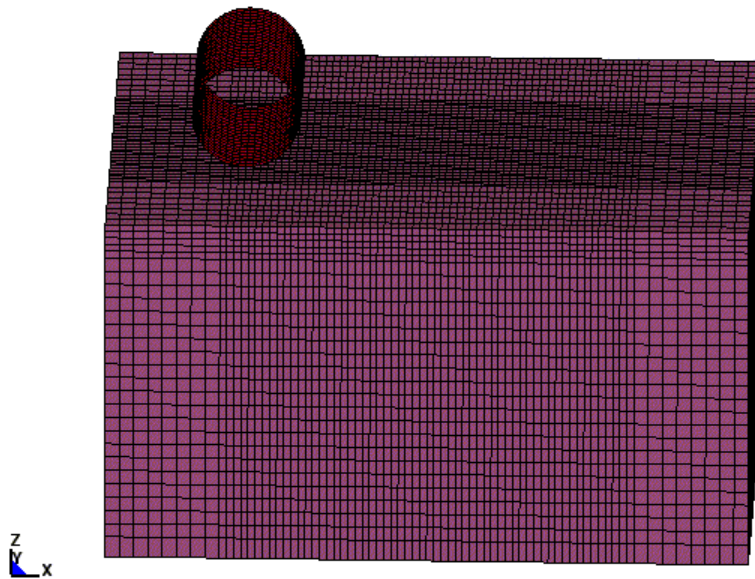
## LANDPAC





# COMPACTION SIMULATION

Time = 0



## COMPACTION

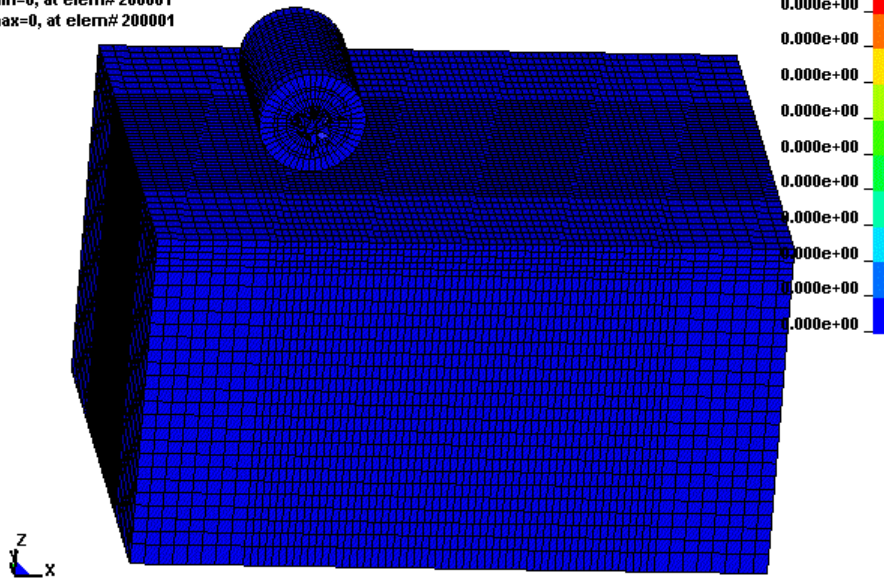
Time = 0

Contours of Z-stress

max ipt. value

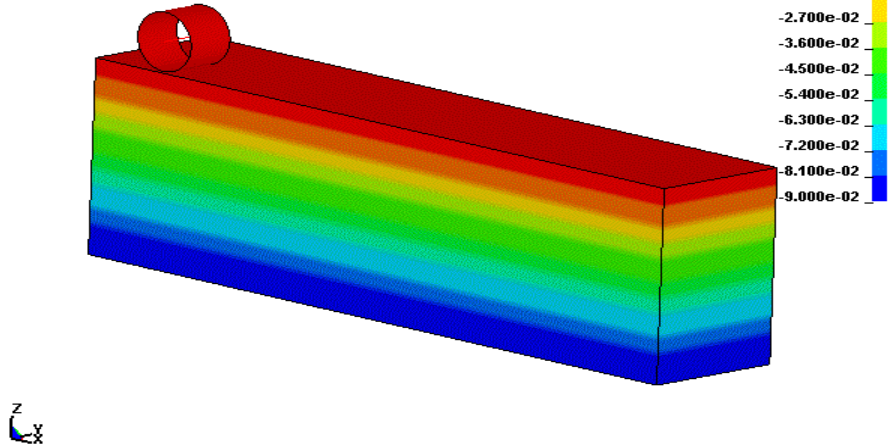
min=0, at elem# 200001

max=0, at elem# 200001





Compaction simulation  
 Time = 0  
 Contours of Z-stress  
 max ipt. value  
 min=-0.0936065, at elem# 2093187  
 max=0, at elem# 1



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Modeling and methodology

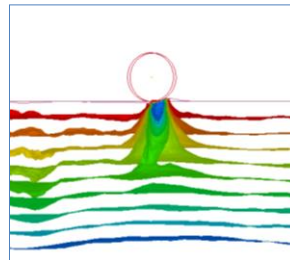
Simulation results



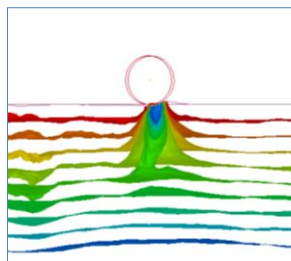
## Visualized Compaction Mechanism

Cylindrical

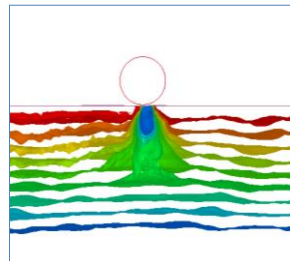
Fringe Levels  
 3.469e-18  
 8.900e-03  
 -1.780e-02  
 -2.670e-02  
 -3.560e-02  
 -4.450e-02  
 -5.340e-02  
 -6.230e-02  
 -7.120e-02  
 -8.010e-02  
 -8.900e-02



$E_s = 10\text{MPa}$



$E_s = 30\text{MPa}$



$E_s = 50\text{MPa}$

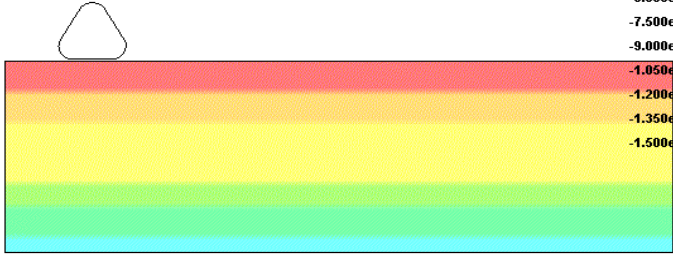
66



# Triangular drum

- LS-DYNA user input  
Time = 0  
Contours of Z-stress  
max ipt. value  
min=-0.0936065, at elem# 2093187  
max=0, at elem# 85

Fringe Levels



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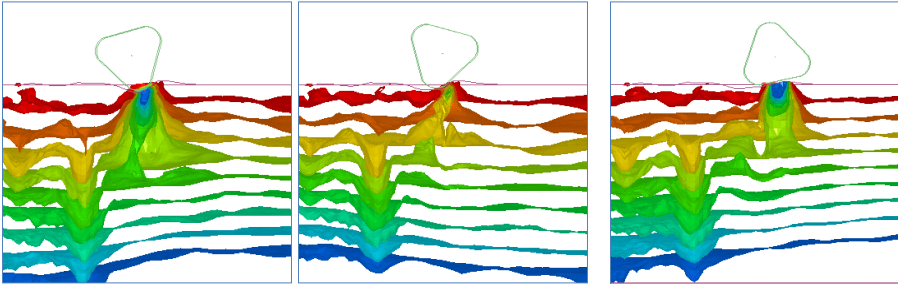
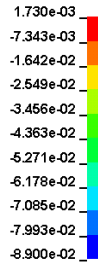


# Visualized Compaction Mechanism(continued)

Triangular

Soil = 10MPa

Fringe Levels

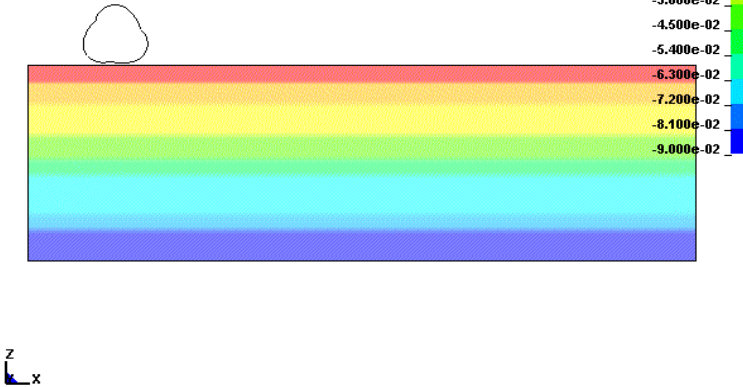


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# Landpac drum

- **Compaction simulation**  
Time = 0  
Contours of Z-stress  
max ipt. value  
min=-0.0936065, at elem# 2093187  
max=0, at elem# 253



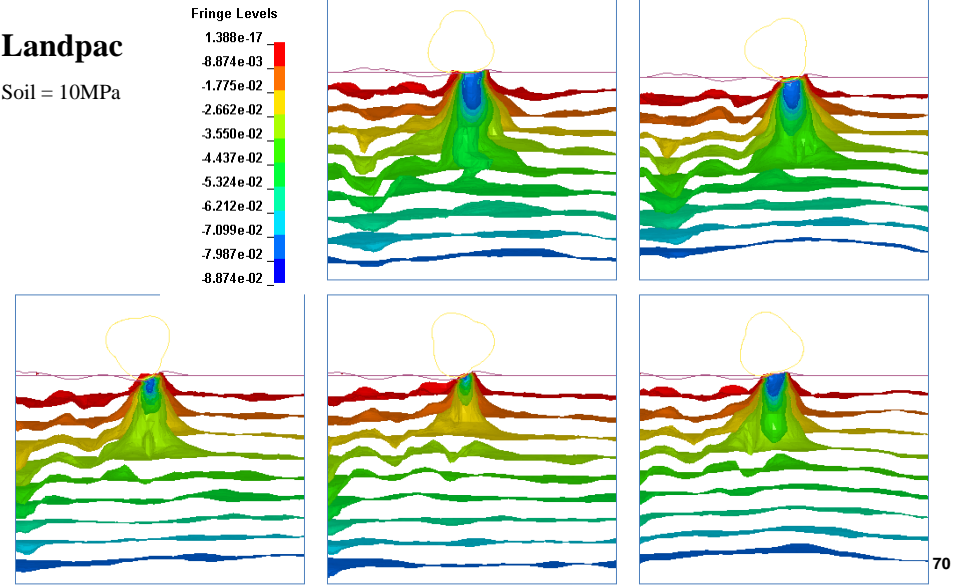
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# Visualized Compaction Mechanism(continued)

## Landpac

Soil = 10MPa



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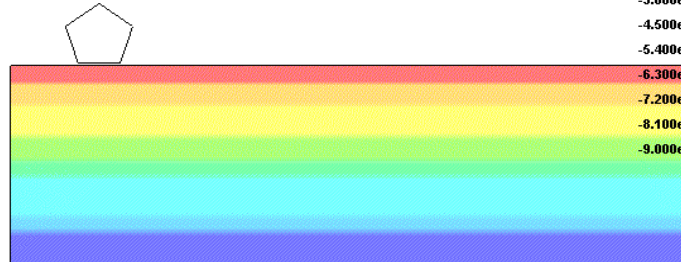
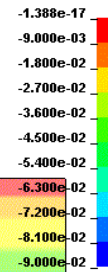


## Pentagonal drum

- Simulation results

Compaction simulation  
Time = 0  
Contours of Z-stress  
max ipt. value  
min=-0.0936065, at elem# 2093187  
max=0, at elem# 641

Fringe Levels



z

71

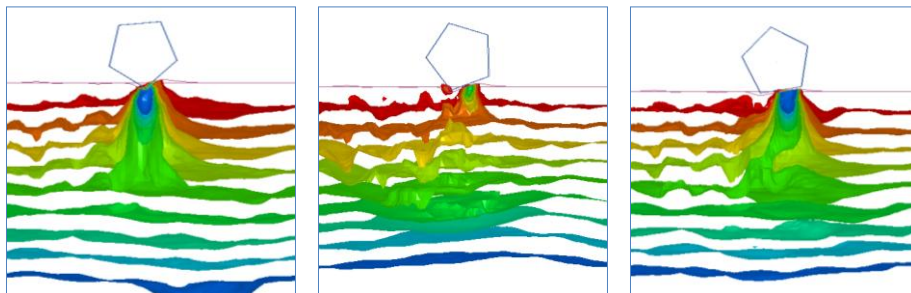
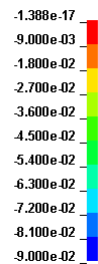


## Visualized Compaction Mechanism(continued)

### Pentagonal

Soil = 10MPa

Fringe Levels



72

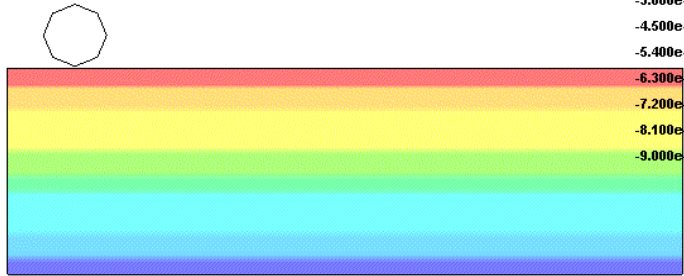
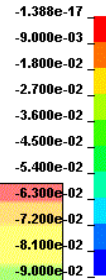


# Octagonal drum

- Simulation results

Compaction simulation  
Time = 0  
Contours of Z-stress  
max ipt. value  
min=-0.085768, at elem# 2164179  
max=0, at elem# 225

Fringe Levels



z

73

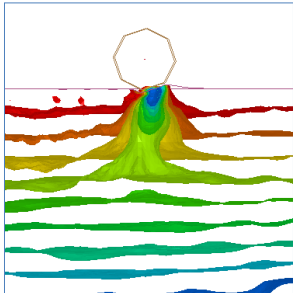
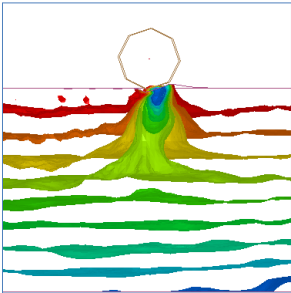
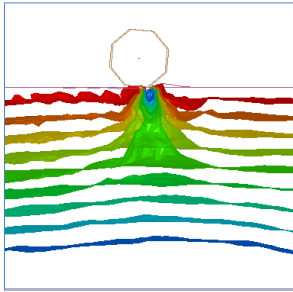
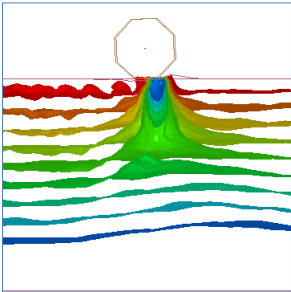
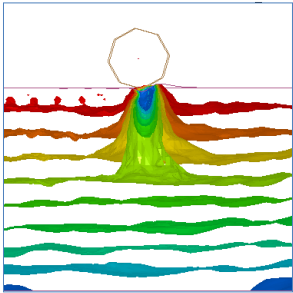
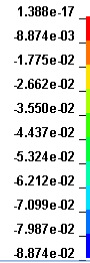


# Visualized Compaction Mechanism(continued)

## Octagonal

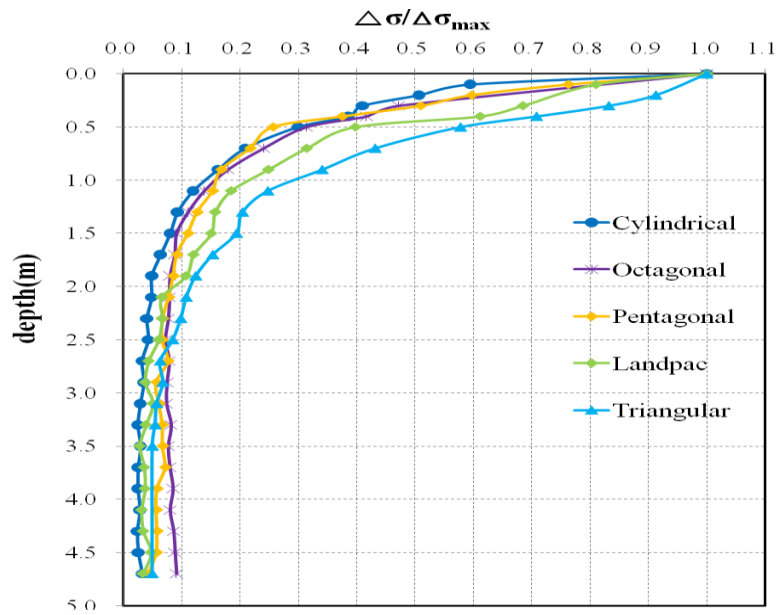
Soil = 10MPa

Fringe Levels



74

Soil Modulus = 10MPa

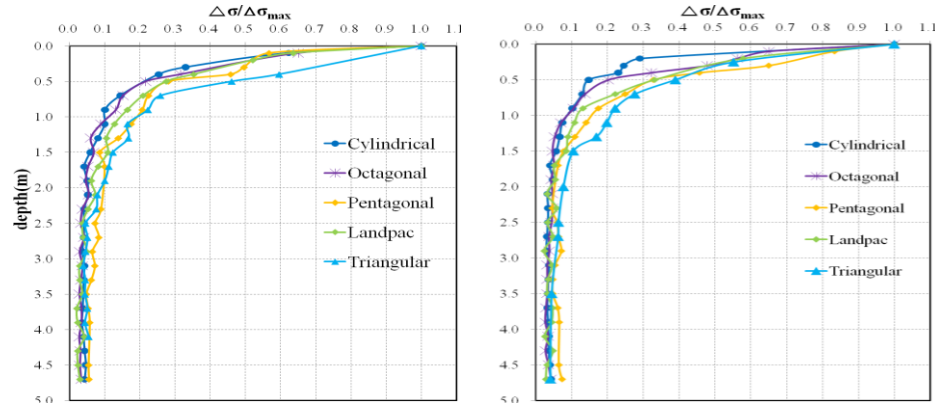


75

Modeling and methodology

Simulation results

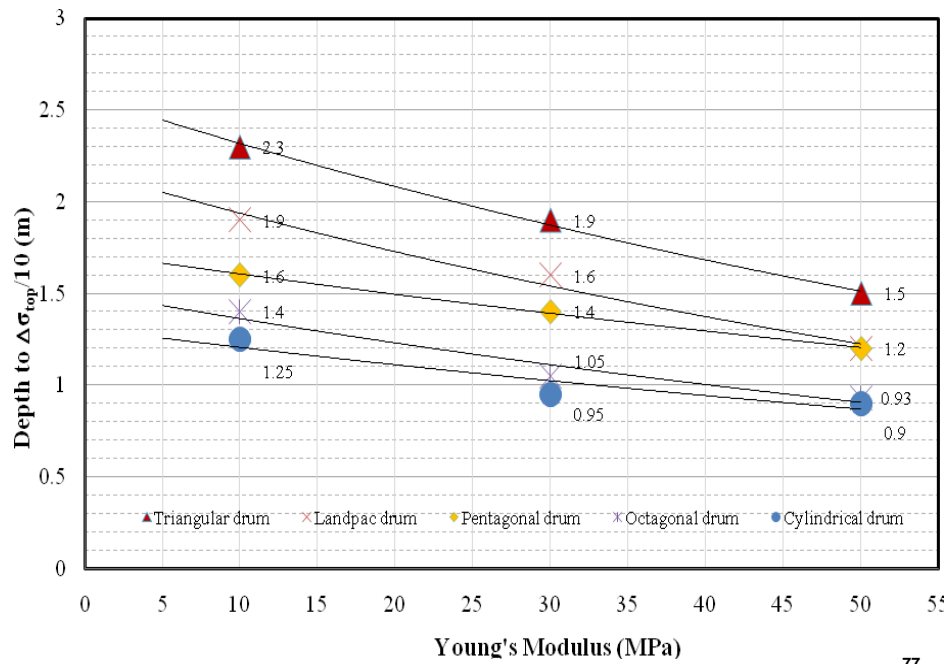
The depth of influence



Soil Modulus = 30MPa

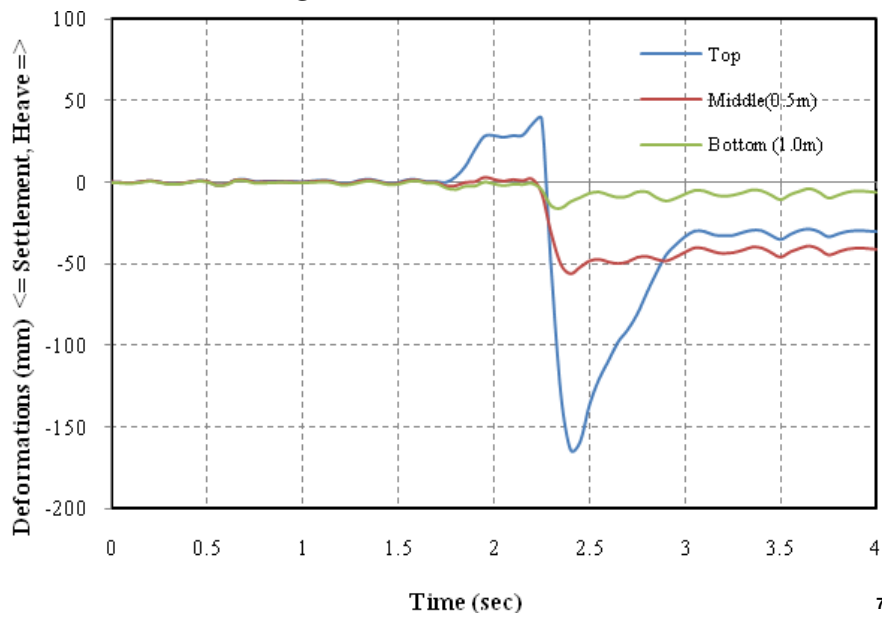
Soil Modulus = 50MPa

76



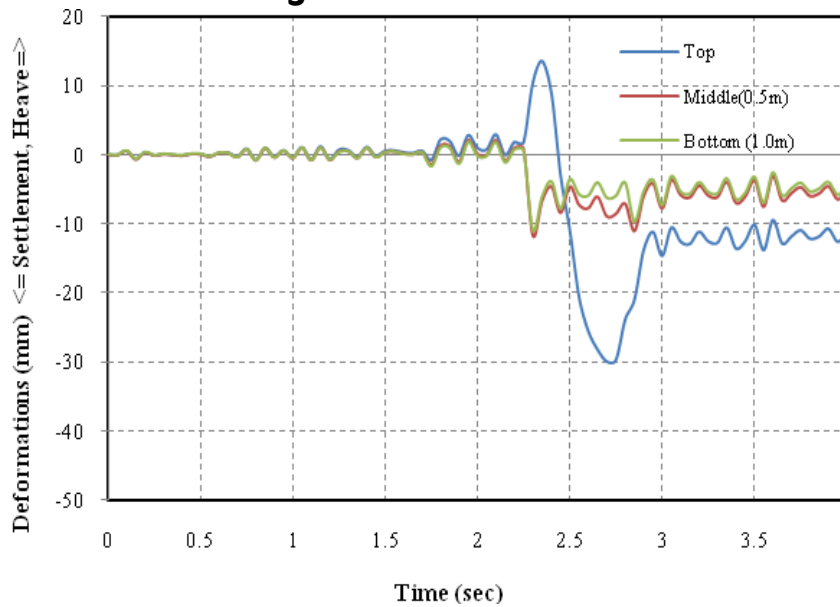
77

**$E_s = 10$  MPa**



78

# $E_s = 50 \text{ MPa}$



79

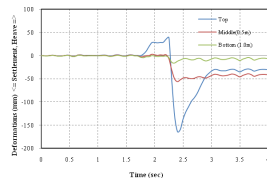
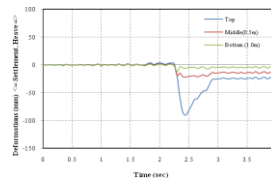
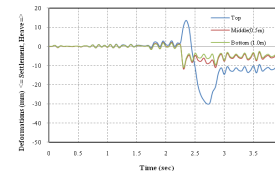
Modeling and methodology

Simulation results

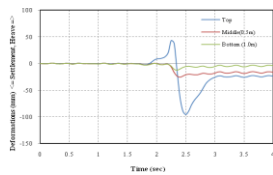
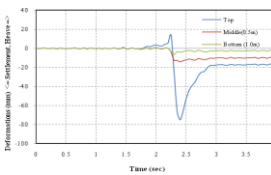
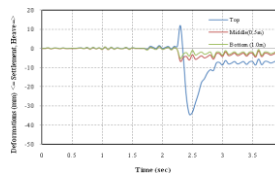


## Surface settlement (continued)

Triangular drum: 32.89mm, 22.82mm, and 10.92mm, respectively

 $E_s = 10 \text{ MPa}$  $E_s = 30 \text{ MPa}$  $E_s = 50 \text{ MPa}$ 

Landpac drum: 26.02mm, 17.28mm, and 8.42mm, respectively

 $E_s = 10 \text{ MPa}$  $E_s = 30 \text{ MPa}$  $E_s = 50 \text{ MPa}$ 

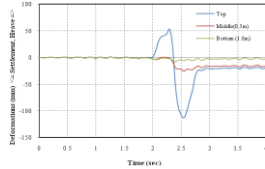
80



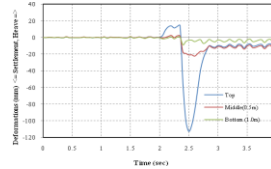
## Surface settlement (continued)



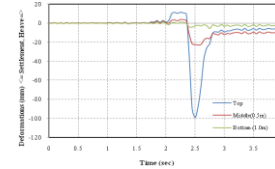
Pentagonal drum: 22.25mm, 14.42mm, and 5.49mm, respectively



$E_s = 10\text{MPa}$

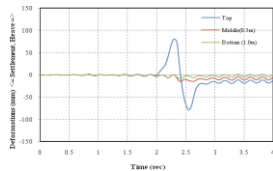


$E_s = 30\text{MPa}$

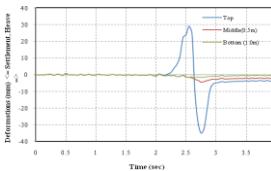


$E_s = 50\text{MPa}$

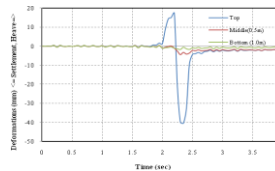
Octagonal drum: 20.13mm, 5.21mm, and 2.26mm, respectively



$E_s = 10\text{MPa}$



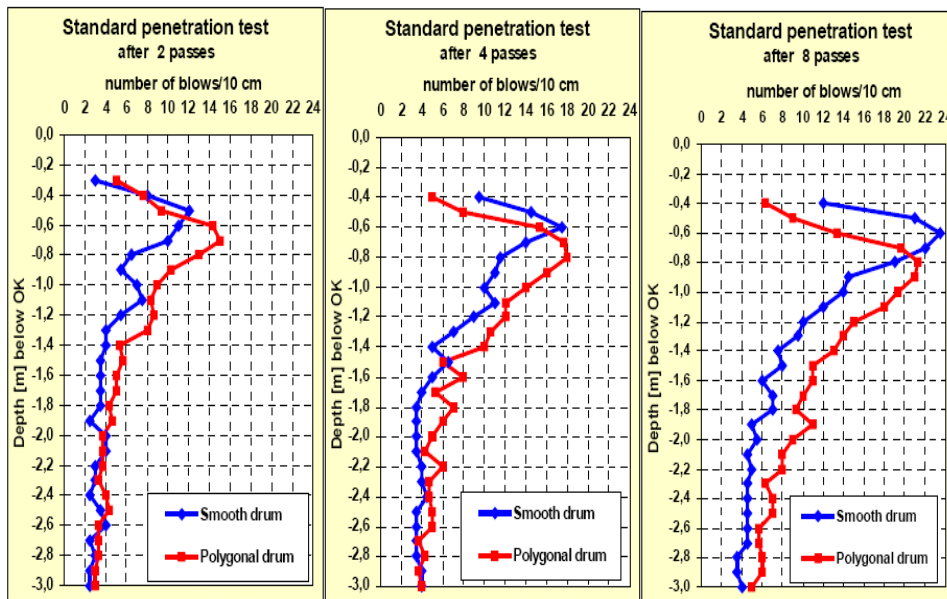
$E_s = 30\text{MPa}$



$E_s = 50\text{MPa}$

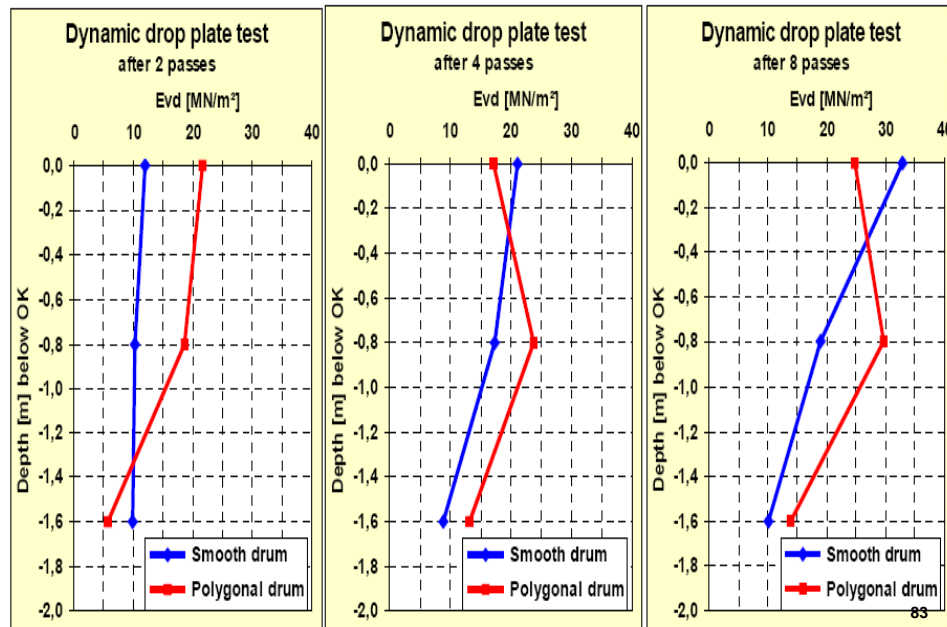
81

## Bomag field test results

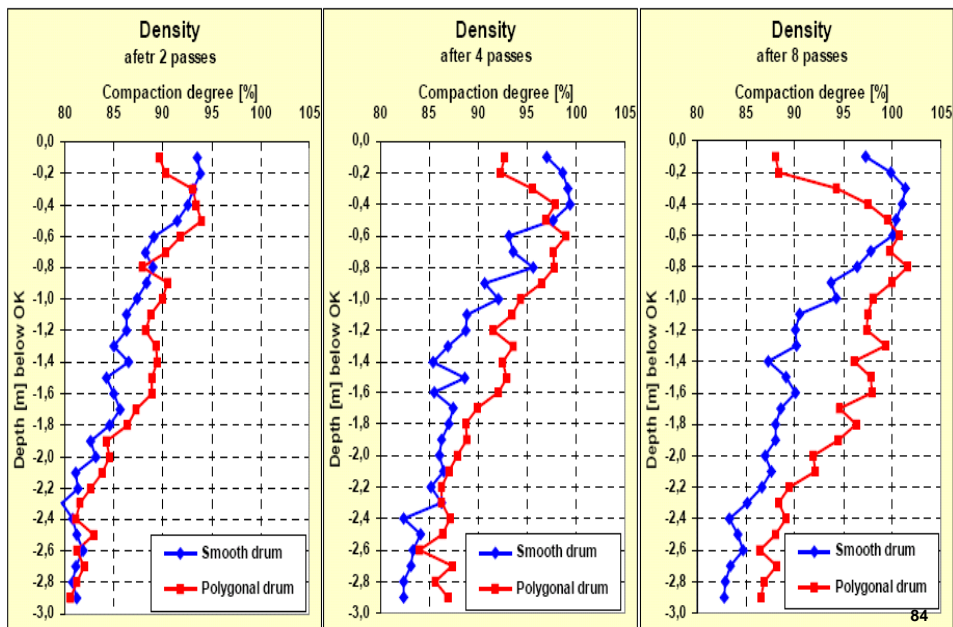


82

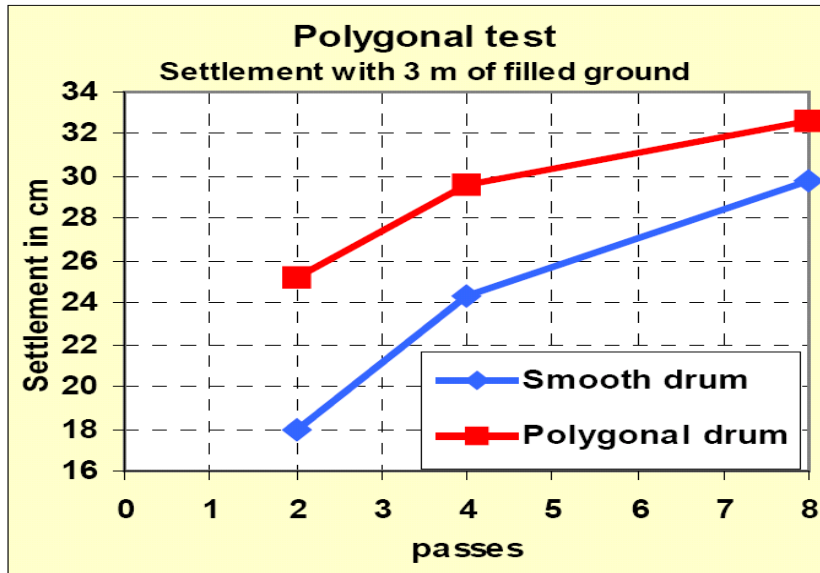
## Bomag field test results



## Bomag field test results

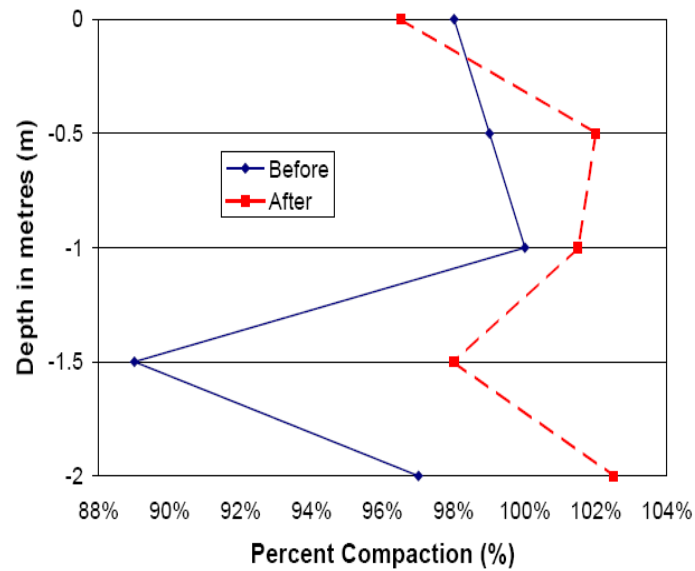


## Bomag field test results



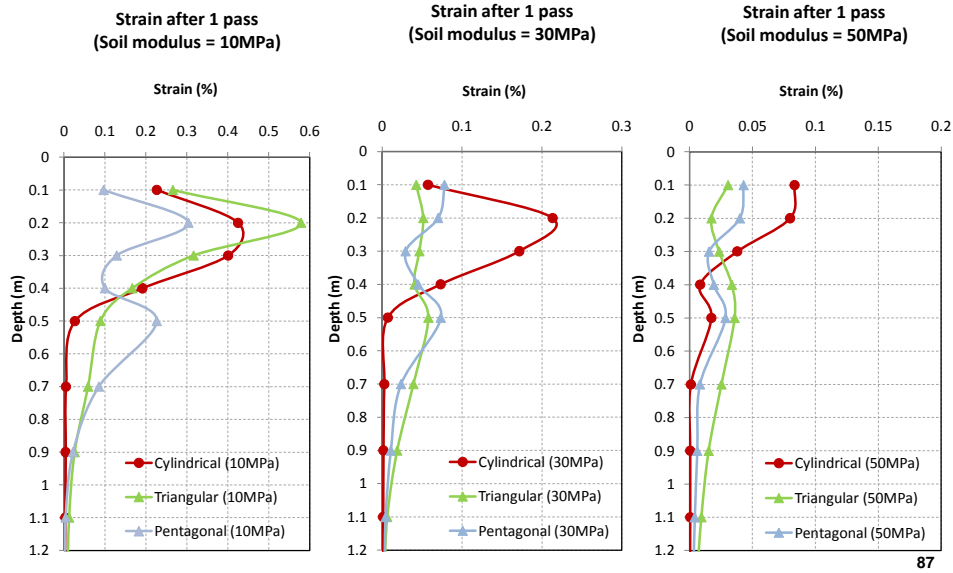
85

## Broons field test results

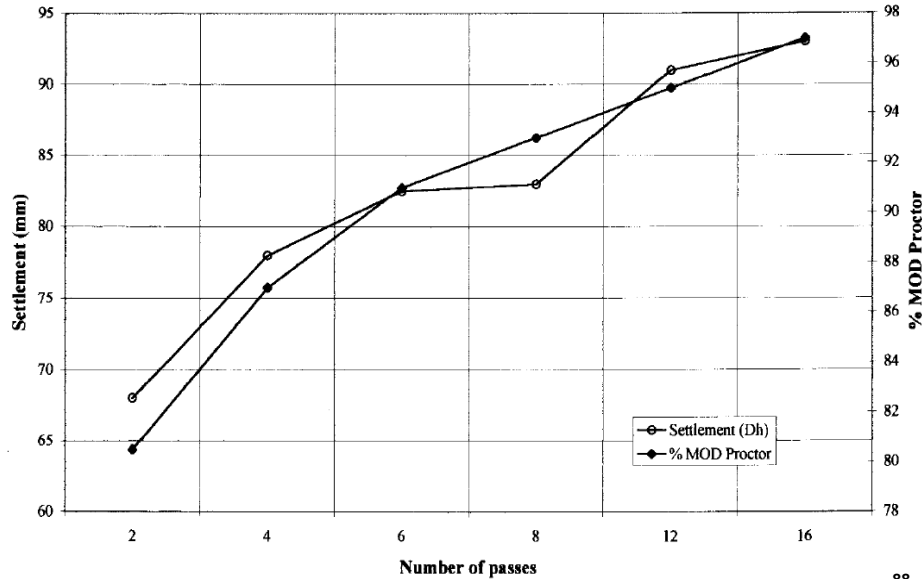


86

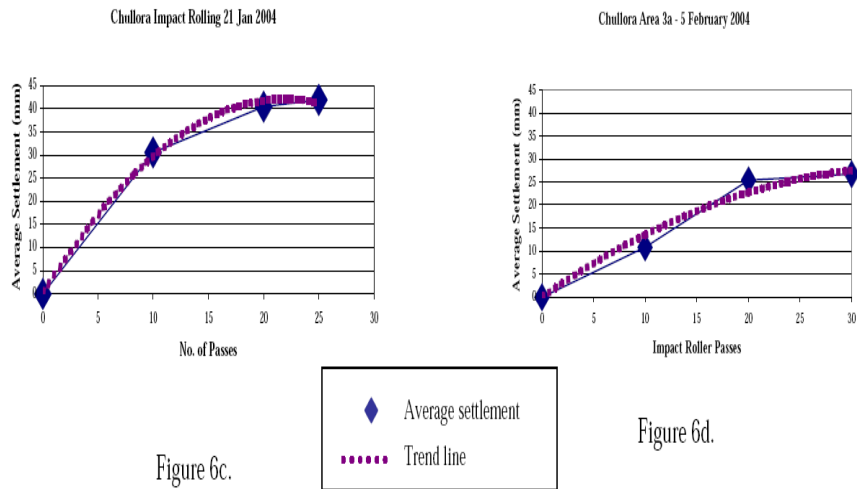
# Texas A&M University simulations



# FORSSBLAD (1980)



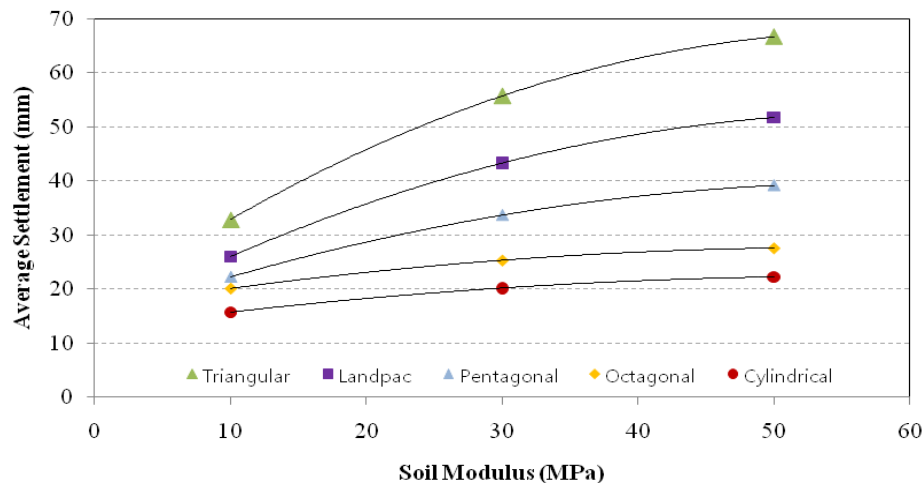
**BROONS FIELD DATA**



89

**Predicted surface settlement**

**Accumulated settlement**



90

## CONCLUSIONS

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- The width of the contact area between the drum and the soil controls the depth of compaction. The softer the soil is, the deeper the roller sinks in the soil, the wider the contact area is, and the deeper the compaction is. Therefore the depth of compaction depends on the stiffness of the soil. As such the depth of compaction decreases with the number of passes.
- The surface pressure controls the degree of compaction. This pressure is higher for the impact rollers than for the cylindrical rollers due to the dynamic effect. Yet the distribution of the pressure is much more uneven for impact rollers than for cylindrical rollers.

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## CONCLUSIONS

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- The depth of compaction is larger for impact rollers because they impart higher stresses which increase the penetration of the roller drum into the soil thereby increasing the width and therefore depth of influence.
- It is also possible that the increase depth of influence is due to wave propagation during the impact. These waves can propagate much deeper than the typical depth of influence for static loading.
- The loosening effect of the surface is more prominent for the impact rollers than for the cylindrical rollers.

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## RECOMENDATIONS

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- Compact first with an impact roller and use several passes to minimize the extent of the areas between impacts.
- Finish by using a cylindrical roller to optimize the compaction of the shallow layers.
- This process combines the benefits of both types of rollers: compaction of the deep layers (0.5 to 1.5 m) with the impact roller but loosening of the shallow layers (0 to 0.5 m) followed by compaction of the shallow layers (0 to 0.5 m) with the cylindrical roller without disturbing the deep layers.

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# THANK YOU

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